



Drag Prediction of Engine-Airframe Interference Effects with CFX 5

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Outline

- CFX the company
- CFX-5 solver technology
- Results AIAA testcases





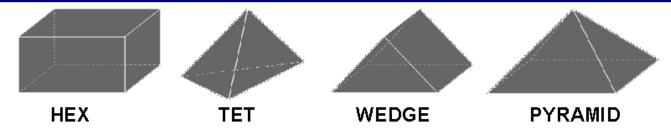
CFX – The Company

- CFX is one of the "big three" CFD companies worldwide
- 200 Full time employees
- **40 Software developers**
- Recently part of ANSYS Inc. (Canonsburg PA)
- General Purpose software with all major models
 - Turbulence, Combustion, Radiation, Multi-phase, Real gas ...
- Applications in all technical areas
 - **Aeronautics and Aerospace**
 - Power generation
 - **Turbomachinery**
 - Transportation ...





CFX-5.6



- Finite volume method for mixed unstructured meshes
- Fully conservative vertex based discretisation
- Co-located variable arrangement (pressure based)
- Fully coupled equation system (mass and momentum coupling)
- Implicit formulation 1st and 2nd order backward Euler
- Rhie & Chow velocity-pressure coupling
- Algebraic multigrid solver
- Scalable parallelisation
- Second order time- and space discretisation
- **Entire Re and Mach number range**

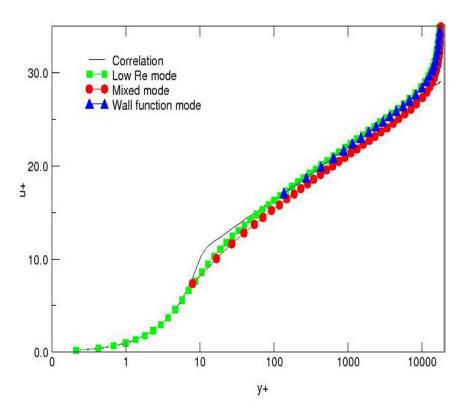




Turbulence Models

- Wide range of turbulence models
 - **One-equation KE1E**
 - Two-equation (k-ε, k-ω, SST ..)
 - RSM (LRR, SSG, SMC-ω,...)
 - LES, DES, SAS
- AIAA drag prediction based on SST model:
 - Reliable separation prediction
 - high accuracy near walls (automatic wall treatment) heat transfer validation
 - Robustness

Automatic Wall Treatment







Testcases

WB – Case

- Single point convergence study (Ma=0.75, Re=3x10⁶, c₁ =0.5, fully turbulent, 3.45m, 5.82m, 10.13m nodes)
- Drag polar a=-3°,-2°,-1.5°,0°,1.0°,1.5° medium grid
- Boundary layer transition specified (P_k=0). Upper 5% at root, 15% at kink, 15% at η=0.844, 5% at tip. Lower 25%



WBNP – Case

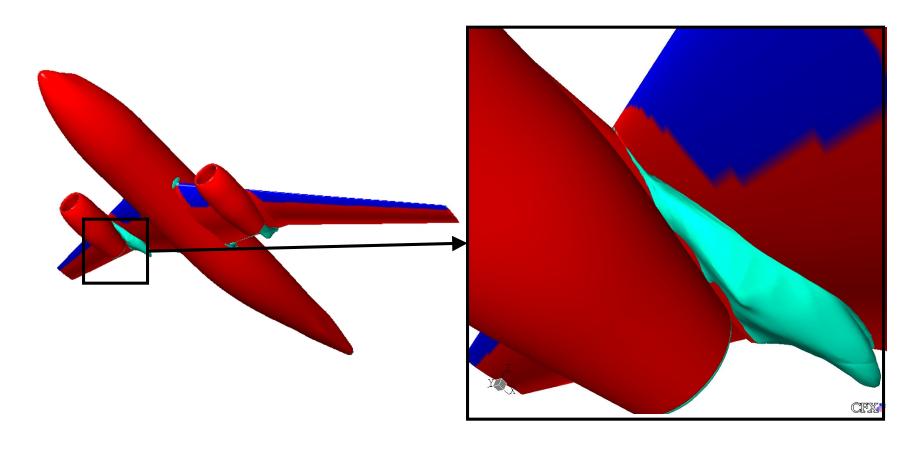
- Single point convergence study (Ma=0.75, Re=3x10⁶, c₁ =0.5, fully turbulent, 4.89m, 8.43m, 13.68m)
- Drag polar a=-3°,-2°,-1.5°,0°,1.0°,1.5° medium grid
- Boundary layer transition specified P_k=0, Upper: 5% at root, 15% at kink, 15% at η=0.844, 5% at tip.
 Lower 25%
- Boundary layer transition critical at wing-pylon intersection – potential for laminar separation at negative angles of attack







CFX Pylon Separation - Transition



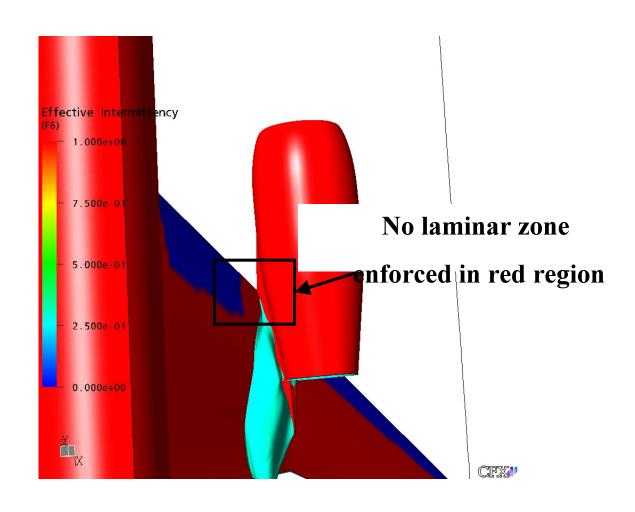
Separated Flow, $\alpha = -2^{\circ}$





CFX Pylon Separation - Transition

- Laminar zone on lower surface was not enforced at wing-pylon intersection
- Otherwise a large separation was observed
- Separation induced transition likely in the experiments







Time Integration

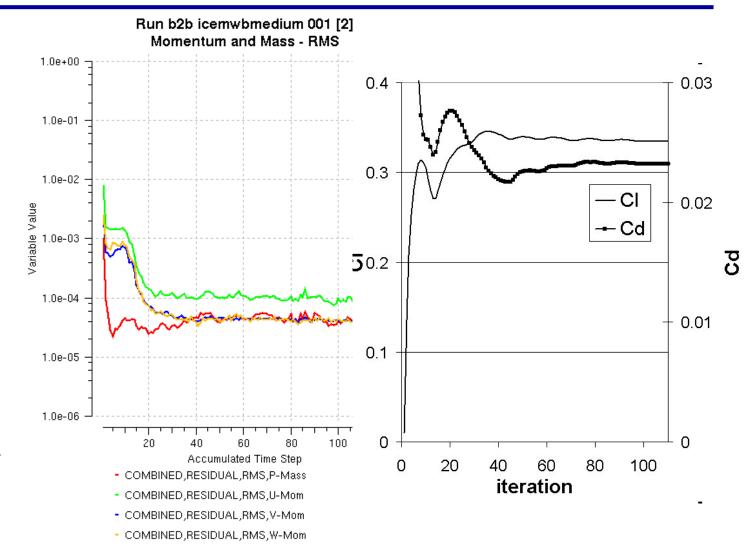
- Solution for most cases would not converge to machine zero.
- For small time steps (∆t~1.x10⁻⁵) unsteady oscillations are observed at the wing-body separated zone.
- Computations carried out in unsteady mode (3) coefficient loops) but with larger time step ($\Delta t=2.x10^{-4}$) to damp unsteadiness.
- Convergence reached in ~120 time steps
- Computing times ~20-24h for 5.82 m nodes on 16 Proc AMD 1900 + Linux cluster.
- Note that steady state simulations are factor 3 faster (no coefficient loops).

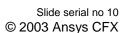




Convergence History

- Unsteadiness
 due to
 oscillating
 separation at
 wing-body
 damped by
 use of large
 time step
 ∆t=2x10-4
- Good convergence in the forces after 100-150 time steps for all cases

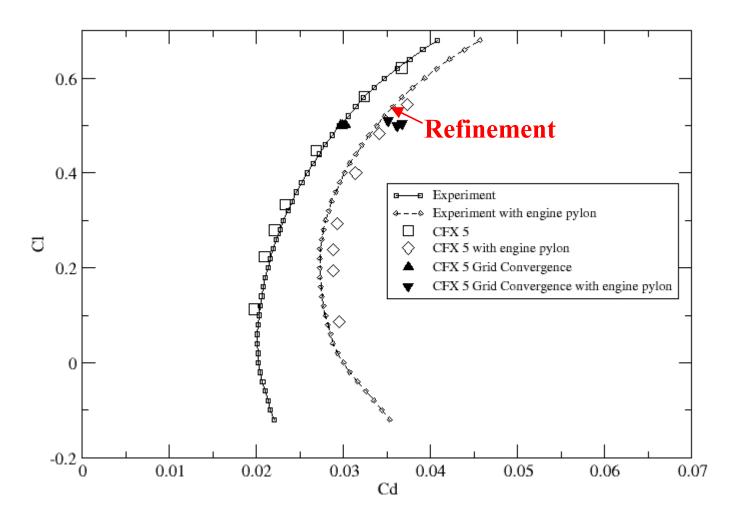








Grid Convergence



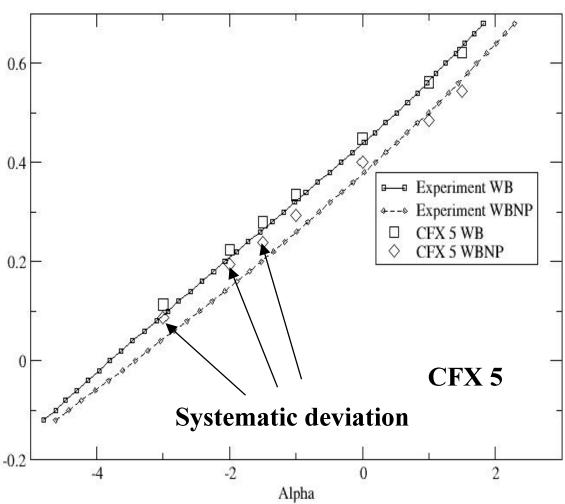




Lift Curve Slope

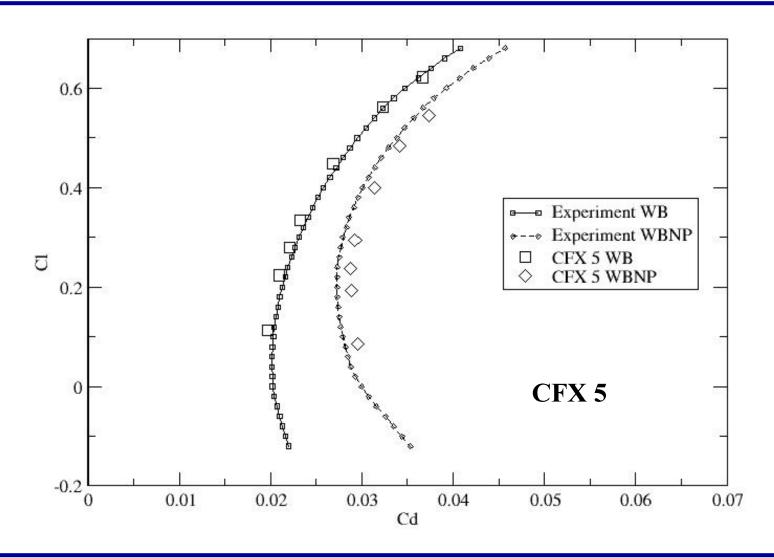


- **Systematic** deviations for negative a for **WBNP** case
 - **Transition?**
 - Wall interference?
 - Also seen in other simulations





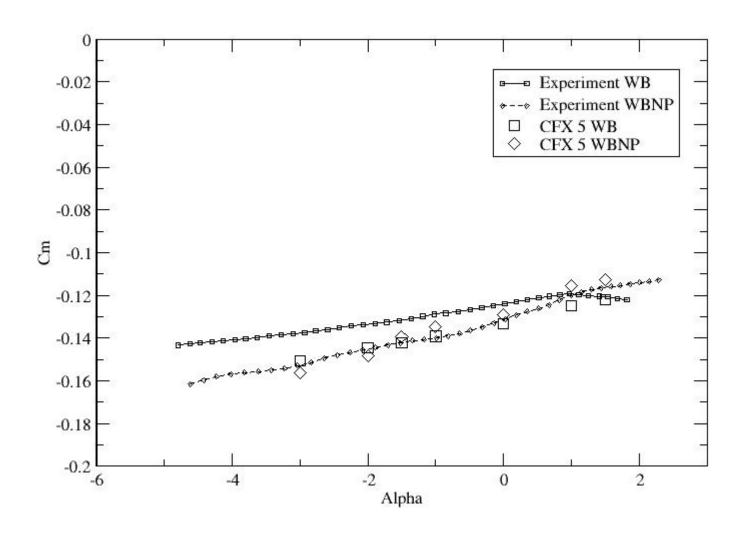
Drag Polar







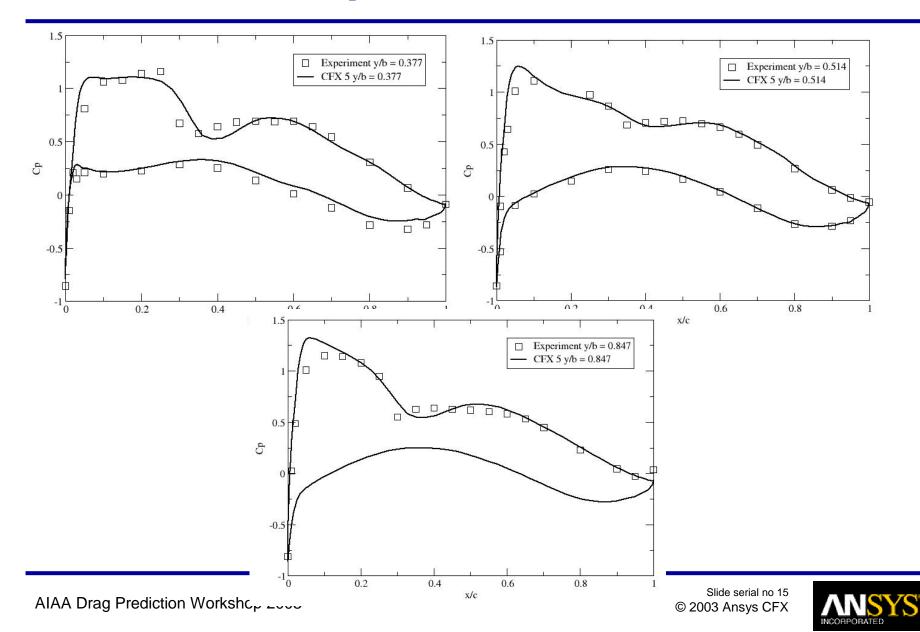
Pitching Momentum





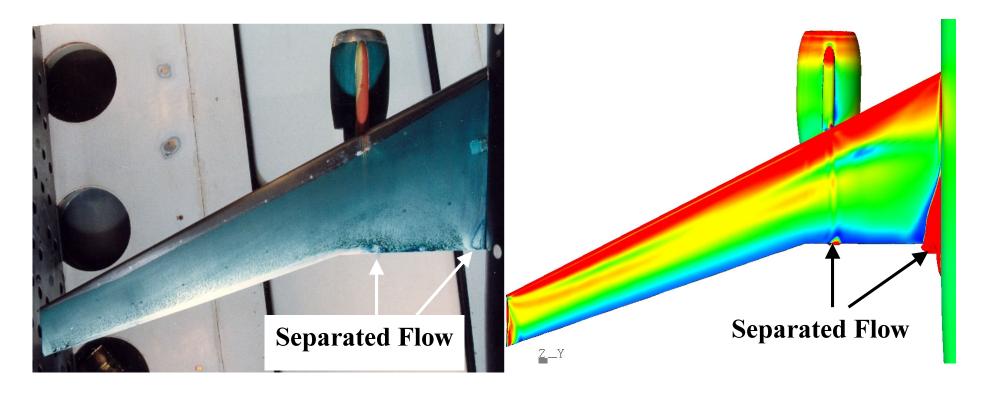


Cp Distributions WBNP





Upper Surface Flow Vis.



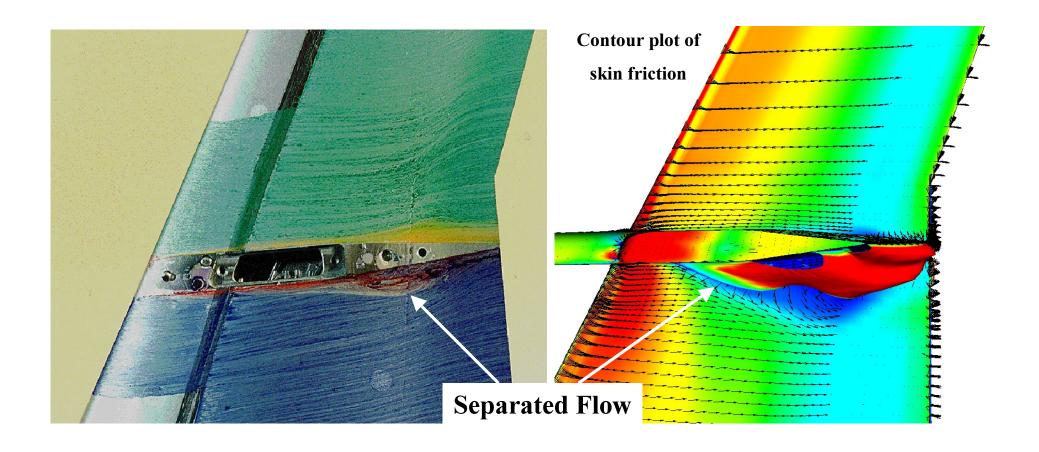
Experimental Oil Flow

CFX 5





Lower Surface Flow Vis.



Experimental Oil Flow

CFX 5





Summary

- Simulations carried out within the Flomania project
- Small grid sensitivity for both cases
- Unsteady simulation performed due to unsteadiness in wing-body separated zone
- Convergence typically in ~120 time steps
- Good agreement with experiments for drag polar for both cases
- Transition location specification problematic for negative α for WBNP case due to separation at the pylon
- Systematic differences for WBNP c₁-α curve at negative α (seen also in other simulations)

